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IMPACT MODIFIED (METH)ACRYLIC POLYMERS

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Abstract

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(54) Title: IMPACT MODIFIED (METH)ACRYLIC POLYMERS

(57) Abstract

A multistage core-shell particle consisting of a core, a first shell and optionally a second shell, substantially free from vinylically unsaturated compounds having at least two equally reactive double bonds, wherein: (i) the core contains a first (meth)acrylic polymer, (ii) the first shell contains a low Tg polymer comprising 0 to 25 % by weight of a styrenic monomer and 75 to 100 % by weight of a (meth)acrylic monomer, the (meth)acrylic monomer capable of forming a homopolymer having a glass transition temperature (Tg) in the range from -75 to -5 °C, and which first shell represents more than 65 % by volume of the combined volume of the core and first shell; (iii) the second shell, when present, contains a second (meth)acrylic polymer which may be the same or different from the first (meth)acrylic polymer; and (iv) the core and first shell together contain from 0.5 to 1.0 % by weight of a graft-crosslinker. A composition and a polysiloxane-free moulded article containing residues obtainable from such core-shell particles. A method of forming a moulding article having improved impact resistance using an impact modifier formed from such core-shell particles.

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Impact Modified (Meth)acrylic Polymers

The present invention relates to impact modified (meth)acrylic polymers and articles formed therefrom.

(Meth)acrylic polymers, for example poly (methyl methacrylate), PMMA, are well known. However, such polymers are often relatively brittle, that is they are not resilient and have poor resistance to sudden impact, thereby limiting their general use.

Conventionally, to improve the impact resistance of such polymers, impact modifying polymers are blended with the (meth)acrylic polymer. These impact modifying polymers typically possess a Tg that is lower than that of the (meth)acrylic polymer and 10 usually a Tg of less than 0°C.

Commonly, the impact modifying polymers are prepared and used in the form of so-called multistage core-shell particles. The multistage core-shell particles are blended, for example melt blended, with the (meth)acrylic polymer to form a composition containing about 40% by weight of the core-shell particles.

15 Extensive activity has centred on achieving the optimum configuration, that is the number and relative thickness of the core and of each shell, and also the composition of the core and of each shell in order to maximise the impact resistance of the resulting blend. Such configurations and compositions have increasingly become more sophisticated and complex thereby leading to increased difficulty and expense of manufacture of the core-shell 20 particles and, hence, the resultant blends. Consequently, impact modified (meth)acrylic polymers are often only used for specialised applications where the need for their superior optical properties outweigh their general expense.

EP-A-0606636 teaches that, in order to achieve improved toughness over that provided for by the addition of an impact modifier in the form of a three stage core-shell, an 25 (meth)acrylic polymer has to be blended with certain specific polysiloxanes. The three stage core-shell particles disclosed consist of an inner core of PMMA which is cross-linked with 1,4 butane diol dimethacrylate; a first shell of a copolymer consisting of 82% w/w of n-butyl acrylate and 18% w/w of styrene; and a second shell of PMMA. The inner core represents 15% w/w of the particle; the first shell 65% w/w of the particle; and the second shell 20% w/w 30 of the particle. The core-shell particles are blended at a level of 40% w/w with a (meth)acrylic polymer. The (meth)acrylic polymer consists of a copolymer containing 99% w/w of methyl methacrylate and 1% w/w of methyl acrylate. The n-butyl acrylate/styrene copolymer content of the blend is calculated as 26% w/w. Improvements in notched impact resistance of up to about 38% are indicated as having been achieved by the additional use of the specified 35 polysiloxanes to achieve a maximum notched impact value of 2.8 kJ.m⁻².

GB-A-2039496 is directed towards the preparation and use of a four stage core-shell particle. Typically, the inner core and second shell are a butyl acrylate/styrene copolymer containing 80% w/w of butyl acrylate, 18% w/w of styrene and 2% of allyl methacrylate graft cross-linker. Typically, the first shell is a methyl methacrylate/ethyl acrylate copolymer 5 containing 94.6% w/w of methyl methacrylate, 5% w/w of ethyl acrylate and 0.4% w/w of allyl methacrylate. The third shell is a methyl methacrylate/ethyl acrylate copolymer containing 95% w/w of methyl methacrylate and 5% w/w of ethyl acrylate. The first and third shells together represent 25% w/w of the particle. Comparative examples show the preparation of a three stage core-shell particle. In the three stage core-shell particle the butyl acrylate/styrene 10 copolymer core has been omitted so that the particles now have a methyl methacrylate/ethyl acrylate core and the methyl methacrylate/ethyl acrylate content of the particles is 25 to 35% w/w. It is shown that, when the particles are blended at a level of 50% with an (meth)acrylic polymer consisting of 95% w/w methyl methacrylate and 5% w/w ethyl acrylate thereby giving a butyl acrylate/styrene copolymer content in the blend of 37.5% w/w (using the four 15 stage core-shell particles) and 27.5% w/w (using the three stage core-shell particles), the four stage core-shell particles gave rise to a 26% increase in impact toughness.

US 5286801 teaches that the impact strength of an (meth)acrylic polymer, consisting of a copolymer containing 99% methyl methacrylate and 1% methyl acrylate, is improved by the use of a five stage core-shell particle in which the core, second shell and 20 fourth shell are formed from a methyl methacrylate/ethyl acrylate copolymer containing 95.4 to 95.8% w/w methyl methacrylate, 3.9 to 4.6% w/w ethyl acrylate and 0 to 0.3% w/w allyl methacrylate; and the first and third shells are a n-butyl acrylate/styrene copolymer containing 80.4% w/w butyl acrylate, 17.6% w/w styrene and 2% w/w allyl methacrylate. The methyl methacrylate/ethyl acrylate copolymer representing 34.5% w/w of the total particle. 25 Comparative examples relate to a three stage core-shell particle in which the core and second shell are formed from a methyl methacrylate/ethyl acrylate copolymer containing 95.9 to 96% w/w methyl methacrylate, 4% w/w ethyl acrylate and 0 to 0.1% w/w allyl methacrylate; and the first shell is a n-butyl acrylate/styrene copolymer containing 80.4% w/w butyl acrylate, 17.6% w/w styrene and 2% w/w of allyl methacrylate. The methyl methacrylate/ethyl acrylate 30 copolymer representing 35.5% w/w of the total particle. When blended at a level of 39% with an (meth)acrylic polymer, to give a n-butyl acrylate/styrene content of 25.5% w/w (using the five stage core-shell particles) and 25.2% w/w (using the three stage particles), the best five stage core-shell particles gave an unnotched Charpy Impact strength of 81 kJ.m⁻² which represented an increase of 19% over that achieved by the comparative three stage core 35 particles.

A C Archer et al, Proceedings of the Churchill Conference on Deformation, Yield and Fracture of Polymers, Cambridge, April 1994, analysed the effect that the number of stages together with the size and content of each stage of various 2 to 4 stage core-shell particles had on the impact strength of (meth)acrylic polymers, as typified by a copolymer 5 containing 92% mol/mol methyl methacrylate and 8% mol/mol butyl acrylate. The general conclusions were that the impact resistance of the blend increased rapidly with increasing volume fraction of n-butyl acrylate/styrene copolymer until the volume fraction was in the range 0.1 to 0.2. However, increasing the volume fraction above 0.2 caused a decrease in impact resistance.

10 Surprisingly, it has now been found that a three stage core-shell particle can be produced which when blended into a relatively brittle (meth)acrylic polymer can imbue the blend with a significantly higher impact resistance than that which has been hitherto achieved with conventional multistage core-shell particles in comparable blends.

Accordingly, in a first aspect, the present invention relates to a multistage core-shell 15 particle consisting of a core, a first shell and optionally a second shell, substantially free from vinylically unsaturated compounds having at least two equally reactive double bonds, wherein

- (i) the core contains a first (meth)acrylic polymer;
- (ii) the first shell contains a low Tg polymer comprising 0 to 25% by weight of a styrenic monomer and 75 to 100% by weight of an (meth)acrylic monomer, the 20 (meth)acrylic monomer capable of forming a homopolymer having a glass transition temperature (Tg) in the range from -75 to -5°C, and which first shell represents more than 65% by volume of the combined volume of the core and first shell;
- (iii) the second shell, when present, contains a second (meth)acrylic polymer which may be the same or different from the first (meth)acrylic polymer; and
- 25 (iv) the core and first shell together contain from 0.5 to 1.0% by weight of a graft-crosslinker.

In a second aspect, the present invention provides a composition comprising a matrix of a third (meth)acrylic polymer containing residues of core-shell particles obtainable from a plurality of multistage core-shell particles consisting of a core, a first shell and 30 optionally a second shell, substantially free from vinylically unsaturated compounds having at least two equally reactive double bonds, wherein

- (i) the core contains a first (meth)acrylic polymer;
- (ii) the first shell contains a low Tg polymer comprising 0 to 25% by weight of a styrenic monomer and 75 to 100% by weight of an (meth)acrylic monomer, the 35 (meth)acrylic monomer capable of forming a homopolymer having a glass transition

temperature, T_g , in the range from -75 to -5°C, and which first shell represents more than 65% by volume of the combined volume of the core and first shell;

(iii) the second shell, when present, contains a second (meth)acrylic polymer which may be the same or different from the first (meth)acrylic polymer; and

5 (iv) the core and first shell together contain from 0.5 to 1.0% by weight of a graft-crosslinker

and in which composition the residues are substantially in the form of two-stage core-shell particles consisting of the core and the first shell.

In a third aspect, the present invention provides a method of forming a moulded 10 article having improved impact resistance which method comprises melt blending a third (meth)acrylic polymer with sufficient of an impact modifier, consisting essentially of a plurality of multistage core-shell particles consisting of a core, a first shell and optionally a second shell, substantially free from vinylically unsaturated compounds having at least two equally reactive double bonds, wherein

15 (i) the core contains a first (meth)acrylic polymer;

(ii) the first shell contains a low T_g polymer comprising 0 to 25% by weight of a styrenic monomer and 75 to 100% by weight of an (meth)acrylic monomer, the (meth)acrylic monomer capable of forming a homopolymer having a glass transition temperature, T_g , in the range from -75 to -5°C, and which first shell represents more than 20 65% by volume of the combined volume of the core and first shell;

(iii) the second shell, when present, contains a second (meth)acrylic polymer which may be the same or different from the first (meth)acrylic polymer; and

(iv) the core and first shell together contain from 0.5 to 1.0% by weight of a graft-crosslinker;

25 to form an impact modified blend containing a volume fraction of the low T_g polymer of at least 0.225 and thereafter moulding the impact modified blend to form a moulded article having an unnotched Charpy Impact strength according to ISO 179-1982(E) of at least 50 kJ.m^{-2} .

In a fourth aspect, the present invention provides a moulded article formed from a 30 composition, which is substantially free of polysiloxanes, comprising a matrix of a third (meth)acrylic polymer and which contains residues of core-shell particles obtainable from a plurality of multistage core-shell particles consisting of a core, a first shell and optionally a second shell, substantially free from vinylically unsaturated compounds having at least two equally reactive double bonds, wherein

35 (i) the core contains a first (meth)acrylic polymer;

(ii) the first shell contains a low Tg polymer comprising 0 to 25% by weight of a styrenic monomer and 75 to 100% by weight of an (meth)acrylic monomer, the (meth)acrylic monomer capable of forming a homopolymer having a glass transition temperature, Tg, in the range from -75 to -5°C, and which first shell represents more than 5 65% by volume of the combined volume of the core and first shell;

(iii) the second shell, when present, contains a second (meth)acrylic polymer which may be the same or different from the first (meth)acrylic polymer; and

(iv) the core and first shell together contain from 0.5 to 1.0% by weight of a graft-crosslinker

10 and wherein the residues are substantially in the form of two-stage core-shell particles consisting of the core and the first shell and are present in sufficient a quantity that the moulded article has an unnotched Charpy Impact strength according to ISO 179-1982(E) of at least 50 kJ.m⁻².

The multistage core-shell particles are preferably spherical in appearance and have 15 an overall diameter, which includes the optional second shell when present, in the range from 250 to 320 nm, and particularly from 270 to 300 nm. Generally, superior optical properties of moulded articles according to the fourth aspect of the present invention are obtained where the overall diameter is in the range from 240 to 260 nm, and particularly about 250 nm.

The core of the multistage core-shell particle preferably has a diameter in the range 20 from 120 to 170 nm, particularly in the range from 120 to 130 nm.

Preferably, the first shell envelopes the core and has a relatively uniform thickness in the range from 50 to 80 nm, particularly in the range 50 to 60 nm, e.g. about 55 nm.

The combination of diameter of the core of the multistage core-shell and thickness of the first shell is chosen such that the first shell represents more than 65% by volume of the 25 combined volume of the volume of the core and first shell. Preferably, the first shell represents at least 75%, particularly at least 80% and especially from 80 to 90%, e.g. about 85% by volume of the combined volume of the volume of the core and the first shell.

The optional second shell preferably envelopes the first shell and serves to improve the handling characteristics of the multistage core-shell particles when in the bulk. In 30 particular the second shell, when present, acts to improve the flow characteristics of the particles.

The first (meth)acrylic polymer is preferably a relatively rigid (meth)acrylate polymer having a glass transition temperature of at least 20°C. Preferred polymers therefore include homopolymers of a monomer selected from C₁₋₄ alkyl methacrylate, i.e. methyl methacrylate, 35 ethyl methacrylate, propyl methacrylate, butyl methacrylate; glycidyl methacrylate; isobornyl

methacrylate; cyclohexyl methacrylate; copolymers containing at least one of the preceding monomers including such copolymers containing a minor proportion of an other monomer selected from at least one C₁₋₄ alkyl acrylate. Particularly preferred first (meth)acrylic polymers are copolymers containing 80 to 99% by weight of methyl methacrylate repeat units 5 and 1 to 20 % by weight of at least one C₁₋₄ alkyl acrylate, especially ethyl and/or butyl acrylate, repeat units. Especially preferred first (meth)acrylic polymers contain about 6% by weight of butyl acrylate which give rise to moulded articles having surprisingly high notched impact strengths.

The second and third (meth)acrylic polymers are preferably selected from the 10 preferred polymers and copolymers of the first (meth)acrylic polymer. Further preferred is for the first and second (meth)acrylic polymers to be selected from the preferred polymers and copolymers. Especially preferred is for the first and second (meth)acrylic polymers to be the same preferred polymer or copolymer.

The (meth)acrylic monomer capable of forming a homopolymer having a glass 15 transition temperature in the range -75 to -5°C is suitably selected from at least one C₃₋₈ alkyl acrylate and/or at least one C₇₋₁₄ alkyl methacrylate. Preferably the (meth)acrylic monomer is capable of forming a homopolymer having a glass transition temperature in the range -65 to -10°C and particularly in the range -65 to -15°C. Preferred (meth)acrylic monomers therefore include butyl acrylate and dodecyl methacrylate.

20 The styrenic monomer, when present, primarily aids in matching the refractive index of the core-shell particle with that of the third (meth)acrylic polymer. In the instance where such matching is not critical then the particular type and amount of styrenic polymer may vary considerably. However, when present, the styrenic monomer preferably constitutes from 14 to 26% by weight and particularly from 16 to 24% by weight of the polymer in the first shell.

25 Where refractive index matching is not critical, relatively low levels of styrenic monomer, e.g. below 14%, preferably from 5 to 10% w/w, can be used to improve the physical performance of moulded articles (as measured by Notched Izod and Unnotched Charpy) at relatively low temperatures, e.g. -20 °C, although the physical performance at the conventional higher testing temperature, i.e. 23 °C, is somewhat diminished.

30 Suitably, the styrenic monomer may be selected from styrene, alpha-methyl styrene, monochlorostyrene, butyl styrene, acrylonitrile and methacrylonitrile. Preferably the styrenic monomer is styrene.

The graft-crosslinker may be selected from the allyl and methallyl esters of acrylic or methacrylic acid. Preferably the graft-crosslinker is allyl methacrylate. The 35 graft-crosslinker may be present at the same percentage by weight in the core and first shell.

Preferably, the core contains from 0.2 to 0.6 % by weight of graft-crosslinker and the first shell contains from 0.8 to 1.2% by weight of graft-crosslinker. Further preferred is that the second shell, when present, does not contain any additional graft-crosslinker.

Although it is commonly viewed that other types of crosslinking agents, such as 5 vinylically unsaturated compounds having at least two equally reactive double bonds, are equivalent to a graft-crosslinker in the present invention such crosslinking agents are not used. Hence, the multistage core-shell particles of the present are substantially free from such crosslinking agents.

The multistage core-shell particles of the present invention may be formed into 10 compositions containing a third (meth)acrylic polymer, as hereinbefore defined. Typically, such compositions are formed by melt blending the core-shell particles with the third (meth)acrylic polymer. In order to achieve significant increases in impact toughness, the volume fraction of the low Tg polymer in the composition is at least 0.225, preferably at least 0.25 and particularly between 0.275 and 0.35. Notwithstanding that significant increases in 15 impact toughness can be achieved, a further advantage of the multistage core-shell particles of the present invention is that conventional levels of impact strength can be achieved using lower amounts of core-shell particles.

Usually, during the formation of the composition, and in particular during the extrusion or moulding of the composition, any second shell that is initially present is stripped 20 from the multistage core-shell particles. Thus, the residues of the multistage core-shell particles in the composition, whether or nor a second shell was initially present, are substantially of the form of two-stage core-shell particles consisting of the original core and first shell. These residues may be identified by applying a suitable stain to a sample of the composition such that the low Tg polymer is shown as a contrasting band against both the 25 core and the third (meth)acrylic polymer. The volume fraction of the low Tg polymer may then be determined from the average thickness of the bands of stained polymer and the number of such bands within a known sampled area.

The compositions may then be used to form moulded articles. The moulded articles possess unnotched Charpy Impact strengths according to ISO 179-1982(E) of at least 50 30 kJ.m⁻², for example at least 60 kJ.m⁻², more typically greater than 70 kJ.m⁻², for example greater than 80 kJ.m⁻², and most usefully in the ranges 80 or 90 to 120 kJ.m⁻². Furthermore, such moulded articles can also show notched Izod strengths according to ISO 180A of at least 3 kJ.m⁻², for example at least 5 kJ.m⁻².

Additionally, when the first (meth)acrylic polymer, which constitutes the core of the 35 multistage particles of the present invention, contains from about 4 to 8% w/w and in

particular from about 4 to 6% w/w, e.g. about 6% w/w, of butyl acrylate is used then moulded articles can be prepared having notched Izod strengths according to ISO 180A of at least 7 kJ.m^{-2} , for example at least 8 kJ.m^{-2} , and more typically from 8 to 10 kJ.m^{-2} . Such compositions also show a surprising improvement on Instrument Falling Weight Impact 5 according to ISO 6603/2 of from below 2 J for compositions containing less than 4% by weight to at least 3 J and particularly at least 3.5 J for compositions containing from 4 to 8% w/w of butyl acrylate. The foregoing improvements in the properties of the moulded articles are unexpected given that the core of the multistage particles is commonly not viewed as that part of the multistage particle which imbues the moulded article with improvements in such 10 physical properties.

As when using conventional compositions, additives such as antioxidants and heat stabilisers may be incorporated with the compositions. However, other impact modifiers, in particular the polysiloxanes of the prior art are not necessary in order to achieve substantially improved impact strengths.

15 The present invention is further illustrated by reference to the following examples.

The multistage core-shell particles were prepared by emulsion polymerisation using the following general protocol.

Seed

Demineralised water (1900 cm³) was added to a 5 litre flask. Seed reagents 20 containing methyl methacrylate monomer, butyl acrylate monomer, allyl methacrylate monomer and Aerosol-OT 75% obtainable from Cytec Ltd were weighed into a glass bottle and then added to the flask. The flask was slowly purged with nitrogen and heated to achieve a stable temperature of 80°C. Potassium persulphate initiator was then added.

After 30 minutes, the seed stage was complete and a sample of approximately 0.5 25 cm³ was pipetted into 4 cm³ of demineralised water for subsequent particle size analysis.

Feed 1

During the seed stage, additional quantities of the reagents in the same proportions as previously used were weighed into a second glass bottle to form Feed 1.

After the seed stage, a further quantity of potassium persulphate initiator was added 30 to the flask and thereafter Feed 1. The flask was continued to be held at 80°C.

After 15 minutes the polymerisation was compete and the core of the core-shell particle had been formed.

Feed 2

During the Feed 1 stage, the reagents required to form the first shell (butyl acrylate, 35 monomer, styrene monomer, allyl methacrylate monomer and Aerosol-OT 75) were

preweighed into a third glass bottle to form Feed 2.

An additional quantity of potassium persulphate initiator was then added to the flask containing the previously formed cores and thereafter Feed 2. As before, polymerisation was conducted at a temperature of 80°C and was complete after 60 minutes to form the first shell 5 of the core-shell particle.

Feed 3

After the Feed 2 stage, the reagents required to form the second shell (methyl methacrylate monomer and butyl acrylate monomer) were preweighed into a fourth glass bottle to form Feed 3.

10 A final quantity of potassium persulphate initiator was then added to the flask and thereafter Feed 3. The polymerisation was again conducted at 80°C and was complete after 15 minutes thereby producing the desired core-shell particles in the form of a polymer latex.

Coagulation

In order to ease the handling of the core-shell particles, a coagulation stage was 15 performed on the polymer latex.

A 10 litre flask was charged with 6 litres of demineralised water to which was added 100g of magnesium sulphate heptahydrate. The contents were then heated to a temperature of 75°C. Whilst agitating the contents under high shear, the polymer latex at a temperature of 80°C was poured into the flask. After addition of the latex, the contents were heated to a 20 temperature of 95°C and held at that temperature for 15 minutes so as to complete the coagulation process.

After coagulation, the polymer was allowed to cool to ambient temperature, for example overnight. The cooled polymer was then dried/washed by centrifugation followed by washing with 4 litres of demineralised water. The drying/washing process was repeated twice. 25 After final centrifugation, the polymer was oven dried at a temperature of 80°C for 24 hours.

Moulding

The dried coagulated polymer was then blended with an appropriate quantity of an injection moulding grade of a (meth)acrylic polymer, which is a copolymer containing 97% w/w of methyl methacrylate and 3% w/w of ethyl acrylate.

30 The resulting blend was then extruded into a lace on a "Clextral" twin screw extruder. A cutter was employed in line with the extruder so as to produce chips suitable for injection moulding.

The chips were injection moulded using a "Demag" toggle-lock machine into test pieces in the form of a HDT bar of dimensions 120 mm x 10 mm x 4 mm and a 4.5 inch 35 (11.43 cm) diameter x 3mm thick disc.

Testing

The HDT bar was used in determining the unnotched Charpy impact performance in a "Zwick" 5102 instrument so as to provide a span of 70 mm, and oriented such that the 4 mm edge was the strike face to receive an impact from a 4 J head.

5 The disc was used in an instrumentated falling weight impact test employing a dart of 12.7 mm falling at a speed of 3m.s⁻¹.

Diameter of Core (nm)	1st Shell Thickness (nm)	1st Shell Content of Core-Shell Particle (% of Volume of Core and 1st Shell)	Graft-crosslinker in Core and 1st Shell is in Range 0.5 - 1.0% by Weight	1st Shell Content of Blend (Volume Fraction)	Unnotched Charpy Impact (kJ.m ⁻²)	Notched Izod Impact (kJ.m ⁻²)
232	8.5	19	N	0.11	11.9	
232	14	29	N	0.15	9.4	
219	15	32	Y	0.16	12.3	
254	19.5	35	Y	0.18	19	
227	19	37	N	0.19	19.1	
230	27.5	47	Y	0.23	24.3	
203	27	51	N	0.24	27.4	
197	28	53	Y	0.25	27.5	
191	28	54	Y	0.25	25.6	
208	31.5	55	N	0.25	14.7	
231	35	55	N	0.26	13.1	
228	37.5	57	Y	0.27	20.2	
195	33	58	N	0.27	29.1	
197	40	64	N	0.29	26.5	
194	48.5	70	N	0.31	26.4	

Diameter of Core (nm)	1st Shell Thickness (nm)	1st Shell Content of Core-Shell Particle (% of Volume of Core and 1st Shell)	Graft-crosslinker in Core and 1st Shell is in Range 0.5 - 1.0% by Weight	1st Shell Content of Blend (Volume Fraction)	Unnotched Charpy Impact (kJ.m ⁻²)	Notched Izod Impact (kJ.m ⁻²)
200	41.5	65	Y	0.29	83.6	
188	45.5	69	Y	0.3	86.6	
195	49.5	71	Y	0.31	97.6	
174	46	72	Y	0.31	92.8	
164	45	73	Y	0.31	111.6	5.99
195	56	74	Y	0.32	92.2	
198	59	75	Y	0.32	91.6	
184	55.5	76	Y	0.32	96.5	
188	59.5	77	Y	0.33	76.5	
159	53.5	79	Y	0.33	85	
175	60	79	Y	0.33	95.5	
190	66	79	Y	0.34	75.2	
157	56.5	80	Y	0.33	96	
183	68	81	Y	0.34	97.3	
149	55	81	Y	0.33	90.7	8.4 *
150	55.5	81	Y	0.33	100	
139	53.5	82	Y	0.33	122.1	6.81
171	67	82	Y	0.34	99	
150	62	84	Y	0.34	100	8.13 *
159	66	84	Y	0.34	97.3	
147	61	84	Y	0.34	84.7	
150	67	85	Y	0.35	98.8	

Diameter of Core (nm)	1st Shell Thickness (nm)	1st Shell Content of Core-Shell Particle (% of Volume of Core and 1st Shell)	Graft-crosslinker in Core and 1st Shell is in Range 0.5 - 1.0% by Weight	1st Shell Content of Blend (Volume Fraction)	Unnotched Charpy Impact (kJ.m ⁻²)	Notched Izod Impact (kJ.m ⁻²)
149	64.5	85	Y	0.35	100	
170	73.5	85	Y	0.35	77.2	
154	70.5	86	Y	0.35	94.6	
152	74.5	87	Y	0.36	74.6	
147	86	90	Y	0.36	88	
109	98.5	95	Y	0.38	79.1	8.97 *
103	105	96	Y	0.38	84.1	9.28 *
108	105.5	96	Y	0.38	81.7	
95	106	97	Y	0.38	88.7	8.73 *

* - indicates the presence of 6 % w/w in the first (meth)acrylic polymer

In a similar manner to the above, further multistage particles were prepared in which the proportion of butyl acrylate in the core and second shell was varied. The multistage particles had cores of about 126 nm in diameter, first shells of about 55 nm in thickness and 5 second shells of about 7 nm in thickness. The first shell therefore represented about 85% by volume of the volume of the core and first shell. The multistage particles were then compounded at 40% by weight as before and the resulting blend used to prepare moulded specimens for testing. The results were as follows:

% by Weight Butyl Acrylate	Falling Weight ISO 6603/2 (J)	Unnotched Charpy Impact (kJ.m ⁻²)	Notched Izod Impact (kJ.m ⁻²)
0	1.9	53	4.2
1	1.4	68	7
4	4.9	82	8.3
6	3.7	75	7.5
8	4.6	82	7

In a similar manner to the above, further multistage particles were prepared having the following composition and dimensions.

Stage	Composition (% w/w)				Diameter (nm)
	Methyl Methacrylate	Butyl Methacrylate	Allyl Methacrylate	Styrene	
Core	93.5	6	0.5	0	148
First Shell	0	90	1	9	275
Second Shell	93.9	6.1	0	0	303

These were then blended as before at 40% by weight and the blend used to prepare specimens for testing. The results of the tests are below and are compared with results obtained from using multistage particles (still within the scope of the present invention) wherein the amount of styrene in the first shell was increased to 18% and the amount of butyl acrylate reduced accordingly.

	9% Styrene in First Shell		18% Styrene in First Shell	
Test Temperature	23 °C	-20 °C	23 °C	-20 °C
Notched Izod (kJ.m ⁻²)	5.6	4.2	9.1	3.8
Unnotched Charpy (kJ.m ⁻²)	77	70	80	57

It can therefore be seen that reducing the amount of styrene in the first shell improves the low temperature characteristics of moulded articles.

Claims

1. A multistage core-shell particle consisting of a core, a first shell and optionally a second shell, substantially free from vinylically unsaturated compounds having at least two equally reactive double bonds, wherein
 - 5 (i) the core contains a first (meth)acrylic polymer;
 - (ii) the first shell contains a low Tg polymer comprising 0 to 25% by weight of a styrenic monomer and 75 to 100% by weight of an (meth)acrylic monomer, the (meth)acrylic monomer capable of forming a homopolymer having a glass transition temperature (Tg) in the range from -75 to -5°C, and which first shell represents more than 10.65% by volume of the combined volume of the core and first shell;
 - (iii) the second shell, when present, contains a second (meth)acrylic polymer which may be the same or different from the first (meth)acrylic polymer; and
 - (iv) the core and first shell together contain from 0.5 to 1.0% by weight of a graft-crosslinker.
- 15 2. A multistage core-shell particle as claimed in claim 1 wherein the first (meth)acrylic polymer is a copolymer containing from 80 to 99% by weight of methyl methacrylate repeat units and from 1 to 20% by weight of at least one C₁₋₁₄ alkyl acrylate repeat units.
3. A multistage core-shell particle as claimed in either claim 1 or claim 2 wherein the first (meth)acrylic polymer contains about 6% by weight of butyl acrylate repeat units.
- 20 4. A multistage core-shell particle as claimed in any one of claims 1 to 3 wherein the (meth)acrylic monomer capable of forming a homopolymer having a glass transition temperature in the range -75 to -5°C is selected from at least one C₃₋₈ alkyl acrylate and/or at least one C₇₋₁₄ alkyl methacrylate.
5. A multistage core-shell particle as claimed in claim 4 wherein the (meth)acrylic monomer is at least one of butyl acrylate and dodecyl methacrylate.
- 25 6. A multistage core-shell particle as claimed in any one of claims 1 to 5 wherein the styrenic monomer is present and constitutes from 14 to 26% by weight of the polymer in the first shell.
7. A multistage core-shell particle as claimed in any one of claims 1 to 6 wherein the 30 core contains from 0.2 to 0.6% by weight of a graft-crosslinker and the first shell contains from 0.8 to 1.2% by weight of the graft-crosslinker.
8. A composition comprising a matrix of a third (meth)acrylic polymer containing residues of core-shell particles obtainable from a plurality of multistage core-shell particles as defined in any one of claims 1 to 7 and in which composition the residues are substantially in 35 the form of two-stage core-shell particles consisting of the core and the first shell.

9. A method of forming a moulded article having improved impact resistance which method comprises melt blending a third (meth)acrylic polymer with sufficient of an impact modifier, consisting essentially of a plurality of multistage core-shell particles as defined in any one of claims 1 to 7 to form an impact modified blend containing a volume fraction of the 5 low Tg polymer of at least 0.225 and thereafter moulding the impact modified blend to form a moulded article having an unnotched Charpy Impact strength according to ISO 179-1982(E) of at least 50 kJ.m⁻².

10. A moulded article formed from a composition, which is substantially free of polysiloxanes, comprising a matrix of a third (meth)acrylic polymer and which contains 10 residues of core-shell particles obtainable from a plurality of multistage core-shell particles as defined in any one of claims 1 to 7 and wherein the residues are substantially in the form of two-stage core-shell particles consisting of the core and the first shell and are present in sufficient a quantity that the moulded article has an unnotched Charpy Impact strength according to ISO 179-1982(E) of at least 50 kJ.m⁻² and a notched Izod strength according to 15 ISO 180A of at least 3 kJ.m⁻².

INTERNATIONAL SEARCH REPORT

International Application No
PCT/EP 96/02216

A. CLASSIFICATION OF SUBJECT MATTER IPC 6 C08F265/06 C08F285/00 C08L51/00 C08L33/04.		
According to International Patent Classification (IPC) or to both national classification and IPC		
B. FIELDS SEARCHED Minimum documentation searched (classification system followed by classification symbols) IPC 6 C08F C08L		
Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched		
Electronic data base consulted during the international search (name of data base and, where practical, search terms used)		
C. DOCUMENTS CONSIDERED TO BE RELEVANT		
Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US,A,4 521 568 (MORI KYOICHIRO ET AL) 4 June 1985 see claim 1; examples ---	1-10
X	EP,A,0 113 924 (RÖHM GMBH) 25 July 1984 see examples -----	1-10
<input type="checkbox"/> Further documents are listed in the continuation of box C.		<input checked="" type="checkbox"/> Patent family members are listed in annex.
<p>* Special categories of cited documents :</p> <p>"A" document defining the general state of the art which is not considered to be of particular relevance</p> <p>"E" earlier document but published on or after the international filing date</p> <p>"L" document which may throw doubt on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)</p> <p>"O" document referring to an oral disclosure, use, exhibition or other means</p> <p>"P" document published prior to the international filing date but later than the priority date claimed</p> <p>"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention</p> <p>"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone</p> <p>"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.</p> <p>"&" document member of the same patent family</p>		
Date of the actual completion of the international search	Date of mailing of the international search report	
4 September 1996	16.09.96	
Name and mailing address of the ISA European Patent Office, P.B. 5818 Patentlaan 2 NL - 2280 HV Rijswijk Tel. (+ 31-70) 340-2040, Tx. 31 651 epo nl, Fax: (+ 31-70) 340-3016		Authorized officer Meulemans, R

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Information on patent family members

International Application No

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